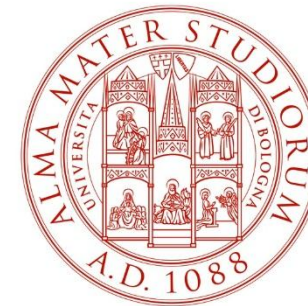




**UNIMORE**  
UNIVERSITÀ DEGLI STUDI DI  
MODENA E REGGIO EMILIA

Dipartimento di Ingegneria  
“Enzo Ferrari”



ALMA MATER STUDIORUM  
UNIVERSITÀ DI BOLOGNA  
DIPARTIMENTO DI INGEGNERIA CIVILE,  
CHIMICA, AMBIENTALE E DEI MATERIALI

# CRT glass management: chemical pretreatment for use in cementitious composites

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# AIM OF THE WORK:

To investigate the effect of a mild chelating agent treatment based on nitrilotriacetic acid (NTA) on the reactivity of funnel glass from waste cathode ray tubes (CRTs) to be used in cement mortars as:

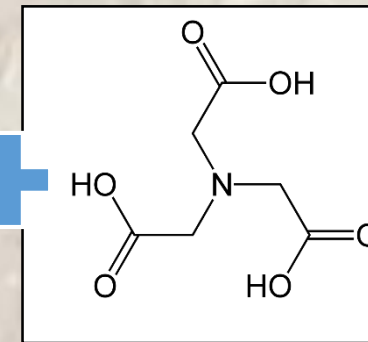
- supplementary cementing material (SCM)
- fine aggregate.



Funnel glass



Nitrilotriacetic acid



CHELATING AGENT  
TREATMENT



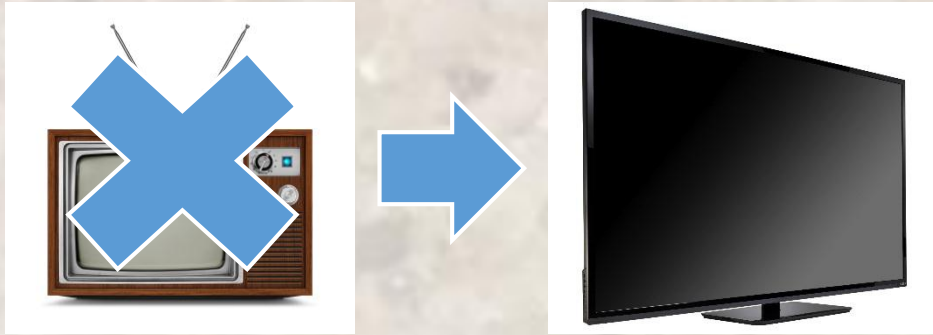
SCM

Treated funnel  
glass in cement  
mortar as:

Sand  
substitute



# Waste CRT monitors



- Italy: **peak quantity in collection** between 2011-2013.
- The **return rate** of TVs and PCs is still the highest among WEEE (65.1 kt collected vs 37.4 kt put on market in 2015).

[Centro di Coordinamento RAEE, Annual Report 2015]



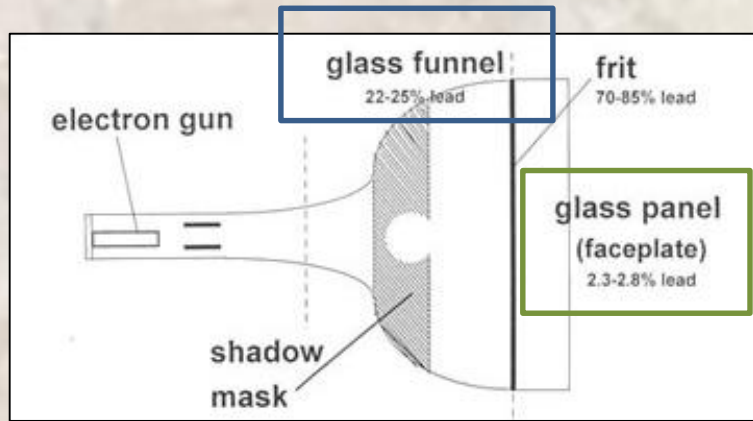
- The **global generation** of waste CRTs was around 6.3 Mt in 2014.
- Most of waste CRTs was generated in Asia (2.5 Mt) followed by Europe and America (1.7 Mt).

[Baldé et al., 2015. *The Global E-Waste Monitor – 2014*. United Nations University, IAS-SCYCLE, Bonn, Germany]



**Urgent disposal problem**

# Funnel glass from waste CRTs



**Panel glass**

BaO (up to 14wt%)  
SrO (up to 12wt%)

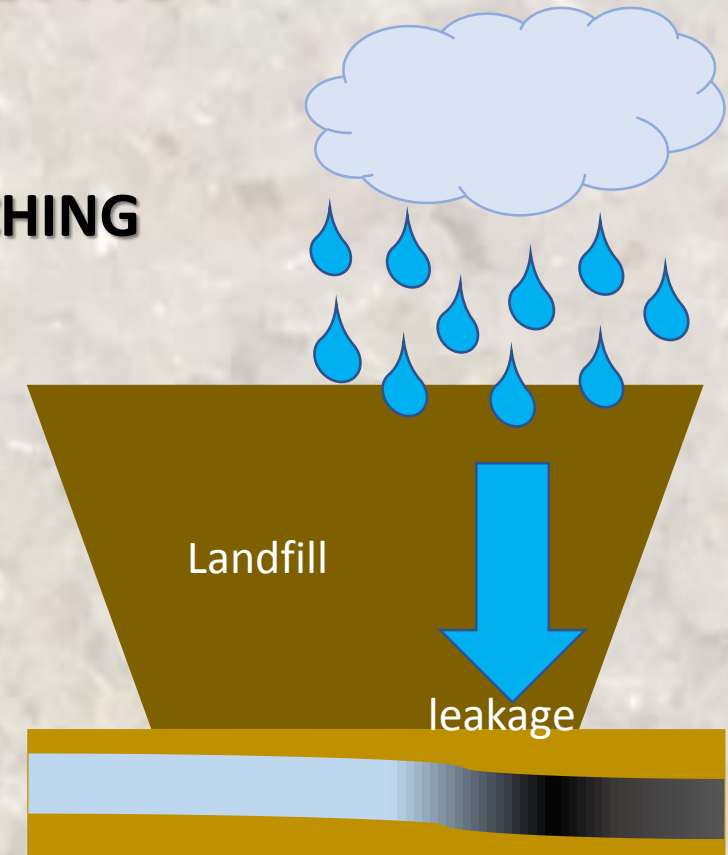
**Funnel glass**

radiation shielding

PbO (12 – 25wt%)



## Pb LEACHING



## RECYCLING PROCESS

Problematic because of:

- Directive 2002/95/EC (RoHS)
  - HIGH ENERGY CONSUMPTION → HIGH COSTS
- (Pb is strongly bonded by encapsulation into the glass matrix)<sup>4</sup>

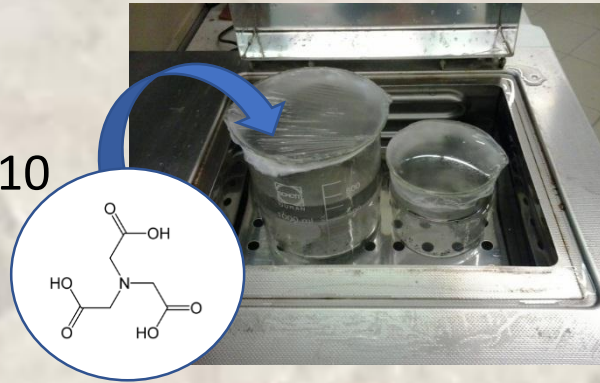


# PROPOSED SOLUTION:

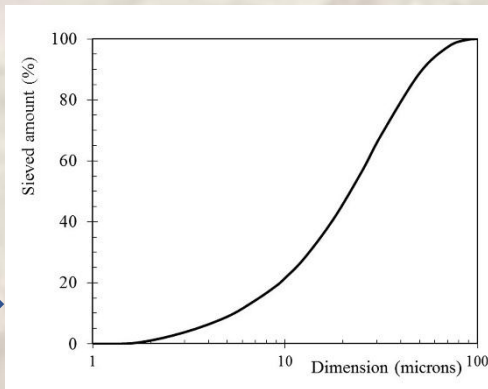
mild chelating agent treatment followed by recycling into cement mortar

## CONDITIONS:

- NTA concentration = 0.1 M
- solid/liquid weight ratio = 1/10
- pH 10
- $T = 80^{\circ}\text{C}$
- $t = 1\text{h}$



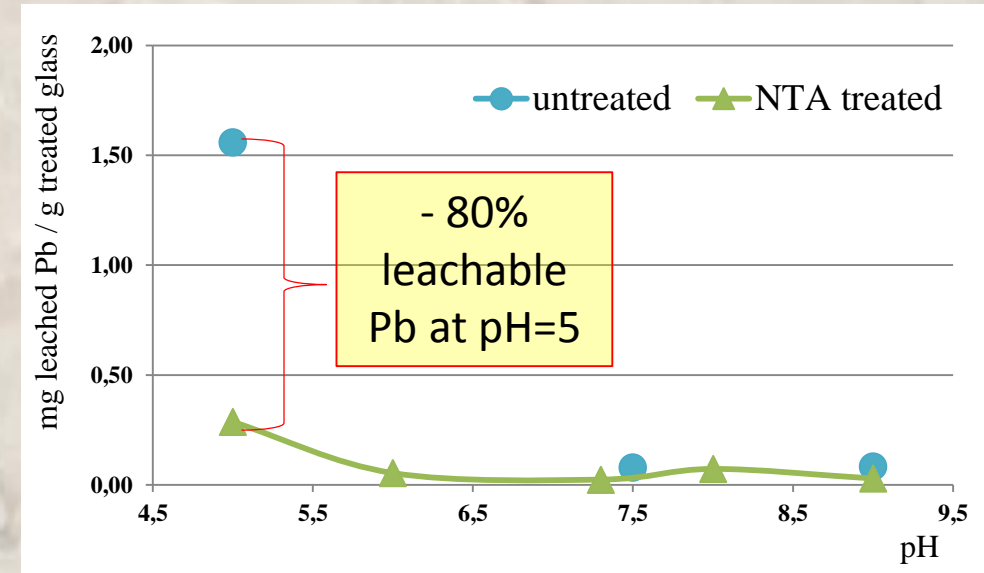
## FNL glass particle size:



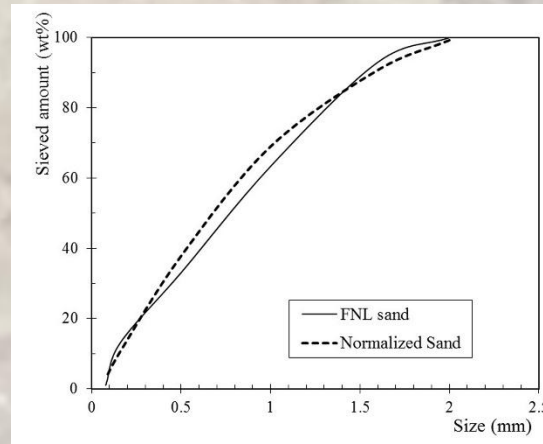
- **SCM:** <100  $\mu\text{m}$

- **Fine aggregate:** 0.075-2.00 mm (distribution close to normalized sand EN 196-1).

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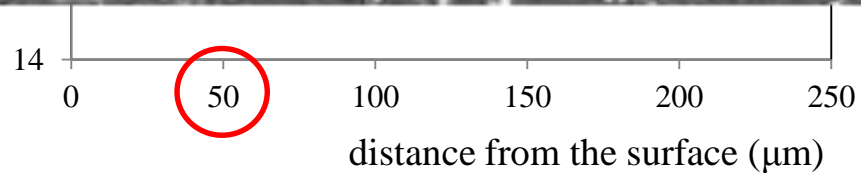
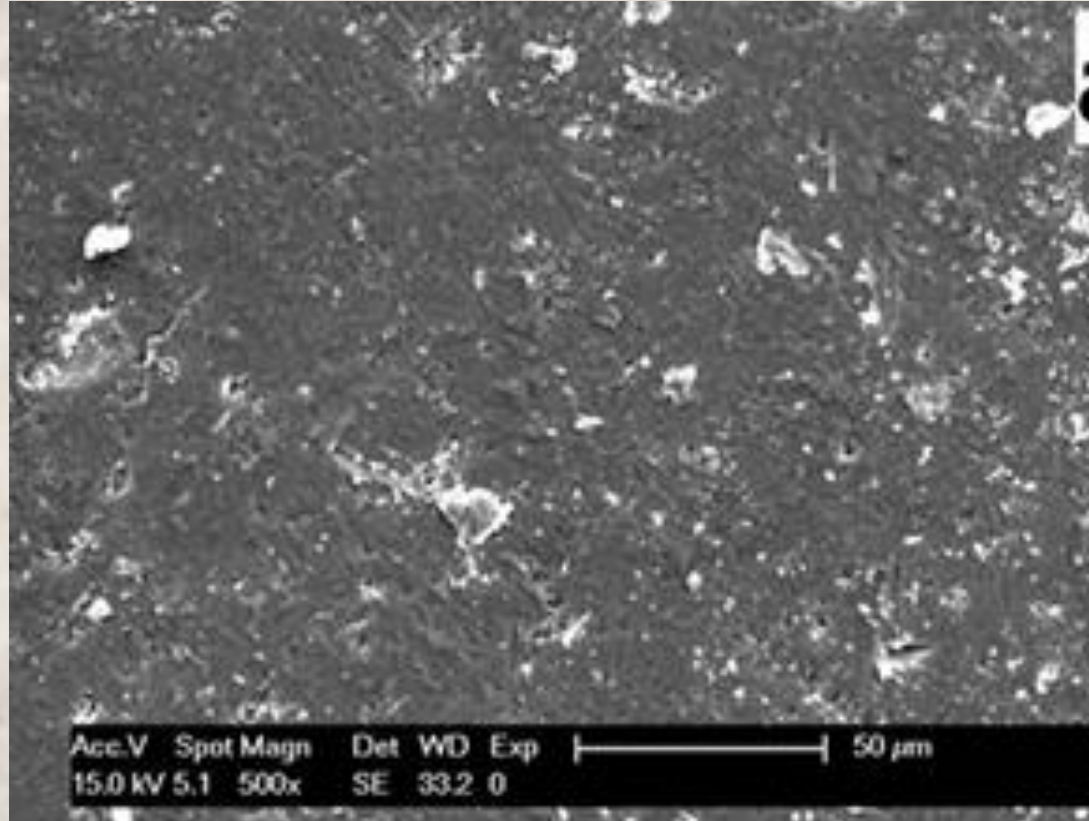


[Bursi et al., 2015. Cathode Ray Tube (CRT) lead glass: lead leaching study after a chelating agent treatment. Environ Eng Manag J]



## Treatment depth analysis

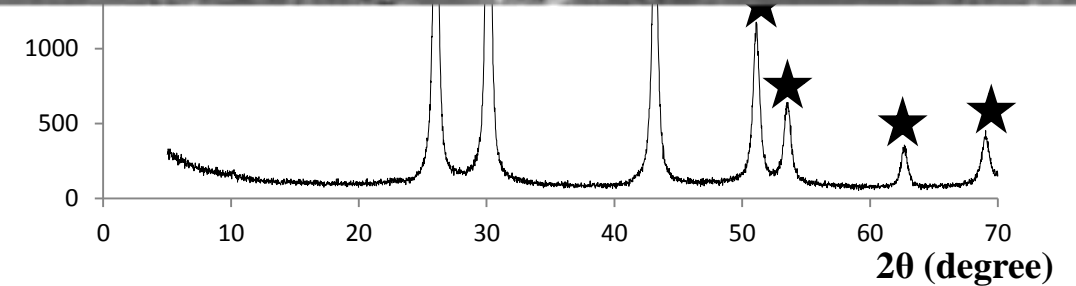
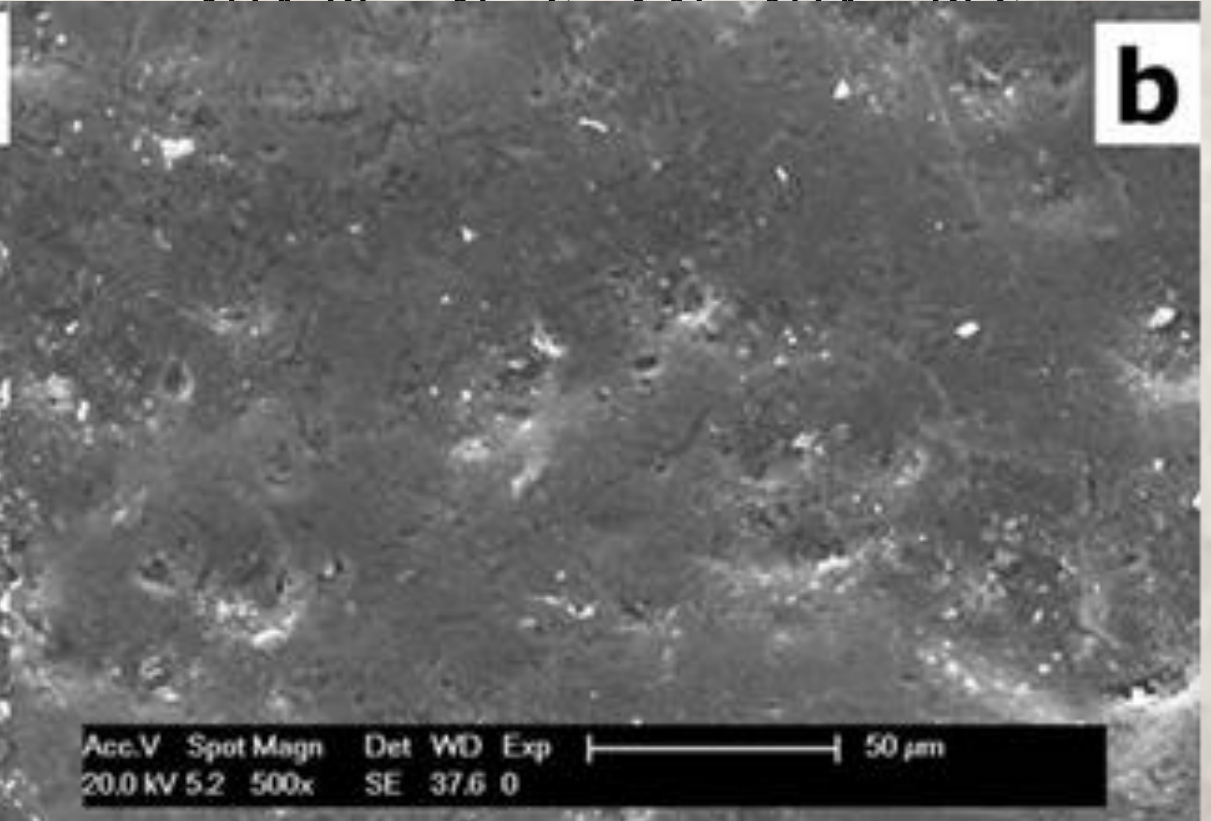
Discoid FNL sample *ad hoc* prepared



Depth of effectiveness < 50 $\mu\text{m}$

## Spent chelating agent solution regeneration

NTA-B/C, NTA-B/C, NTA-B/C, NTA-B/C



XRD spectrum of PbS precipitate



# Mortars preparation

BINDER: CEM I 52.5 ( $\text{Na}_2\text{O}$  equivalent of 0.75%)

AGGREGATE: standard siliceous sand (EN 196)

## CASTING ACCORDING TO EN 196-1

$a/b = 3/1$

$w/b = 0.50$

**AMOUNT OF SUBSTITUTED CEMENT OR SAND = 25wt%.**  
(both NTA-treated and untreated FNL glass were used)

**CURING** → 24 h; 100 % R.H.; 25°C



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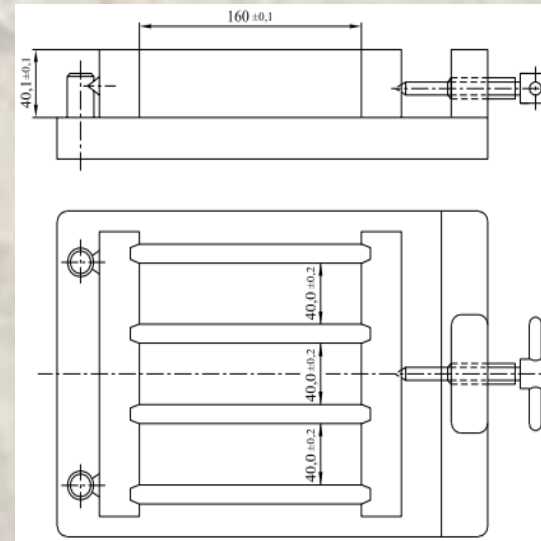
Glass addition (both as SCM and sand) slightly increased mortars workability → 10% higher slump (EN 196)



Mortars mixing



Mortars' mould



Mould geometry

## UNTREATED FNL (XRF)

Oxide	wt%
$\text{SiO}_2$	55.15
$\text{PbO}^*$	17.98
$\text{K}_2\text{O}$	5.84
$\text{Na}_2\text{O}$	9.13
$\text{Al}_2\text{O}_3$	2.96
$\text{CaO}$	2.51
$\text{BaO}$	2.16
$\text{MgO}$	1.82
$\text{SrO}$	1.02
Br	0.39
$\text{Sb}_2\text{O}_3$	0.17
$\text{ZnO}$	0.14
$\text{ZrO}_2$	0.15
$\text{Cr}_2\text{O}_3$	0.01
$\text{Fe}_2\text{O}_3$	0.09
$\text{TiO}_2$	0.08
$\text{NiO}$	0.13

# Experimental test

## Glass solubility test:

- Alkaline attack (pH=12) with  $\text{NaOH}+\text{Ca}(\text{OH})_2$  solution,  $l/s=60$ ,  $80^\circ\text{C}$ , 28 h
- Analysis by EDS

## Glass and mortars leaching test (EN 12457-2):

- Sample ground and sieved under 4 mm
- Leaching in distilled water,  $l/s=10$ , T room, 24 h, under stirring
- Analysis by ICP-OES

## Mechanical test:

- 1) Compression on mortars (EN 196-1)
  - Curing  $\rightarrow 25^\circ\text{C}$ , R.H. 100%
  - Testing machine: 100 KN Wolpert, speed test 50 mm/min
- 2) Activity Index (EN 450-1)

## Expansion test ASR (ASTM C1260 and ASTM C227):

- $a/b= 2.25/1$
- Curing  $\rightarrow 80^\circ\text{C}$ , NaOH solution (mortars)
- Analysis by mechanical comparator

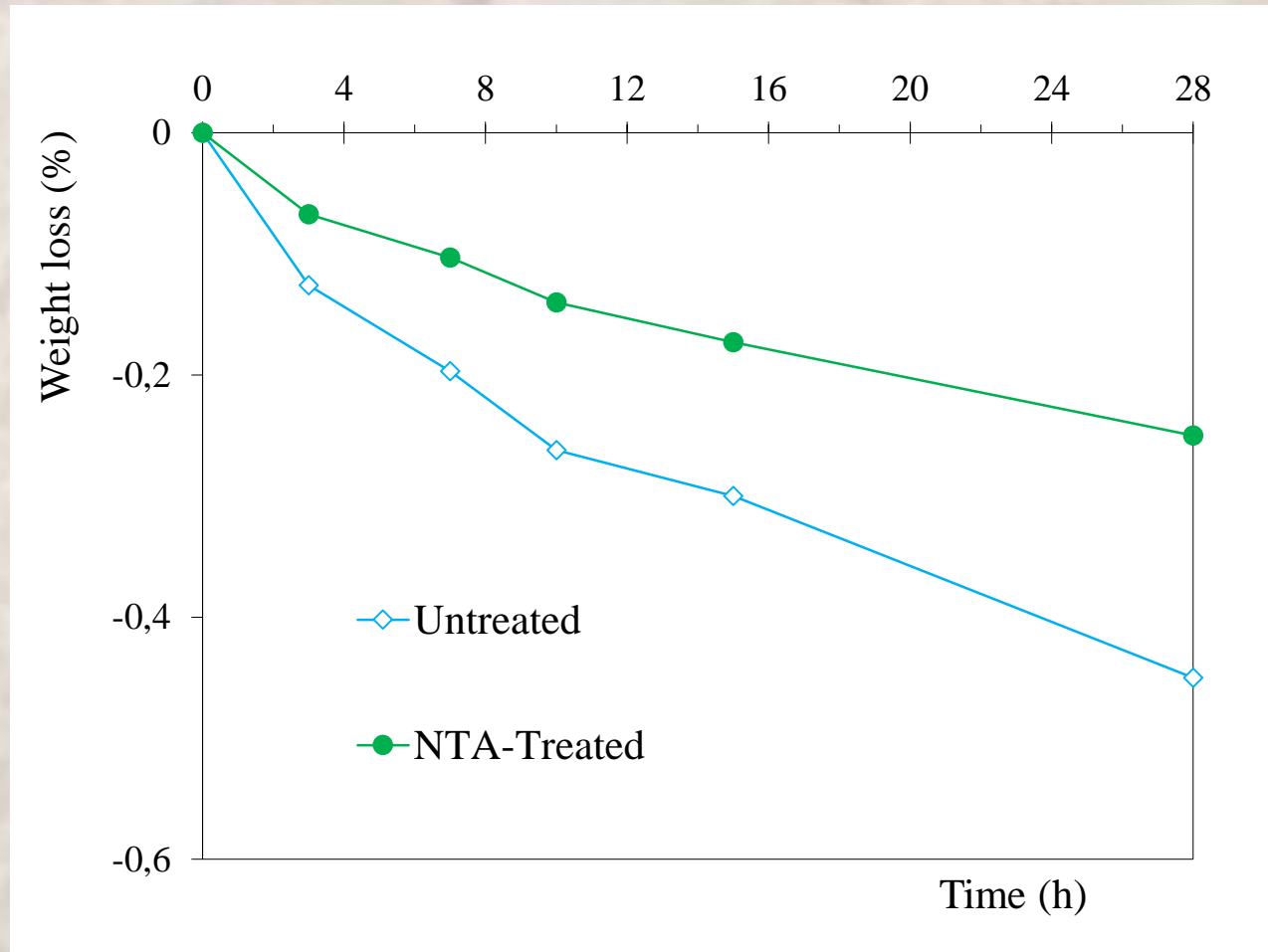


compression test



# Solubility test

(alkaline attack (pH=12) with NaOH+Ca(OH)<sub>2</sub> solution, l/s=60, 80°C, 28 h)



## WEIGHT LOSS:

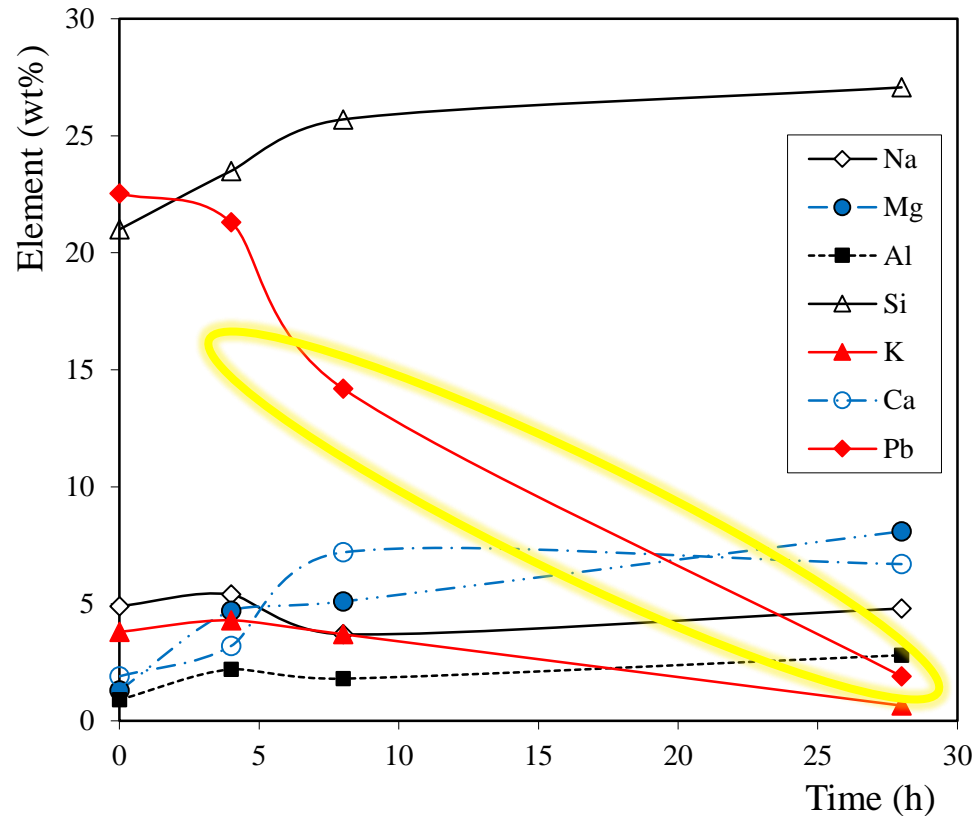
By decreasing Pb amount on the outer surface, FNL glass becomes less soluble.

This behaviour confirms:

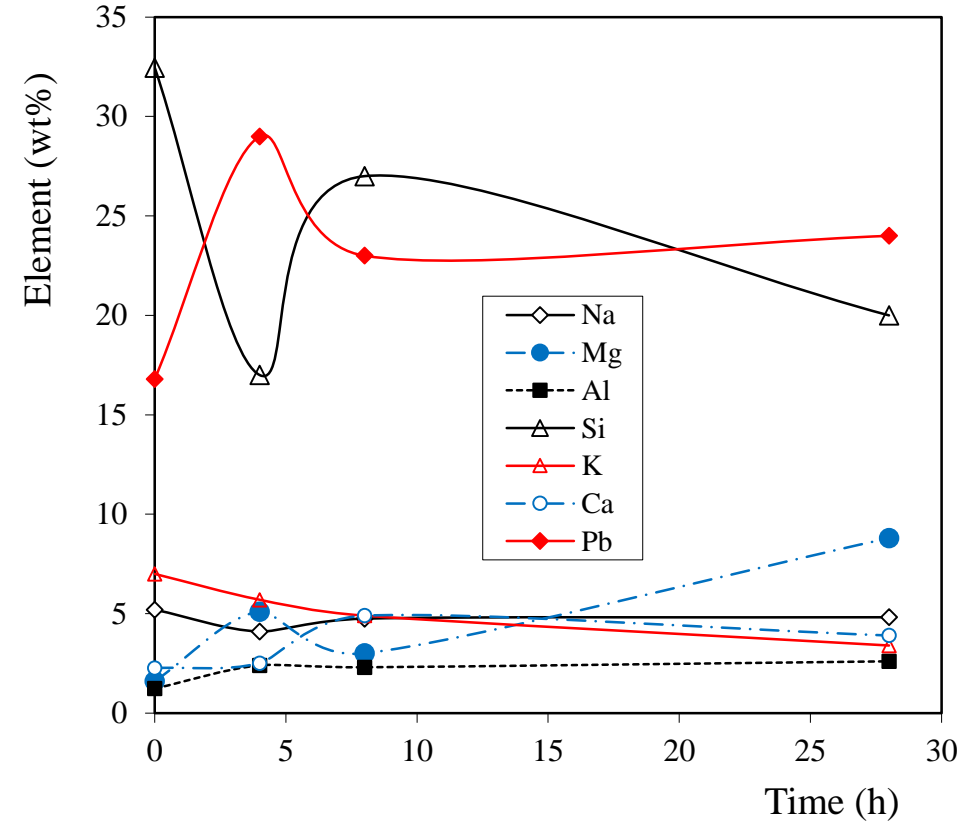
- the relatively poor resistance of Pb glass to alkaline solutions (Volf, 1984);
- that Pb behaves as a NETWORK MODIFIER when <50wt%. (Schultz-Münzenberg et al., 1998)

# Solubility test

## UNTREATED



## NTA-TREATED



- A steady and progressive dissolution of Pb and K (soluble cations, **network modifiers**) takes place.
- Ca and Mg (**stabilizing oxides** in glassy network) are almost constant.

- Smaller variation of elemental composition takes place (less solubility of NTA-treated glass).



# Leaching test

(EN 12457-2)

	NTA-FNL SCM	FNL SCM	NTA-FNL aggregate	FNL aggregate	NTA-FNL glass	FNL glass
Pb (mg/L)	< 0.1	< 0.1	< 0.1	< 0.1	< 0.1	< 0.1



In all the samples the Pb concentration resulted to be ten times **under the limit** for acceptance in landfills for non-hazardous waste, namely 1 mg/L (EU Landfill Directive 1999/31/EC)



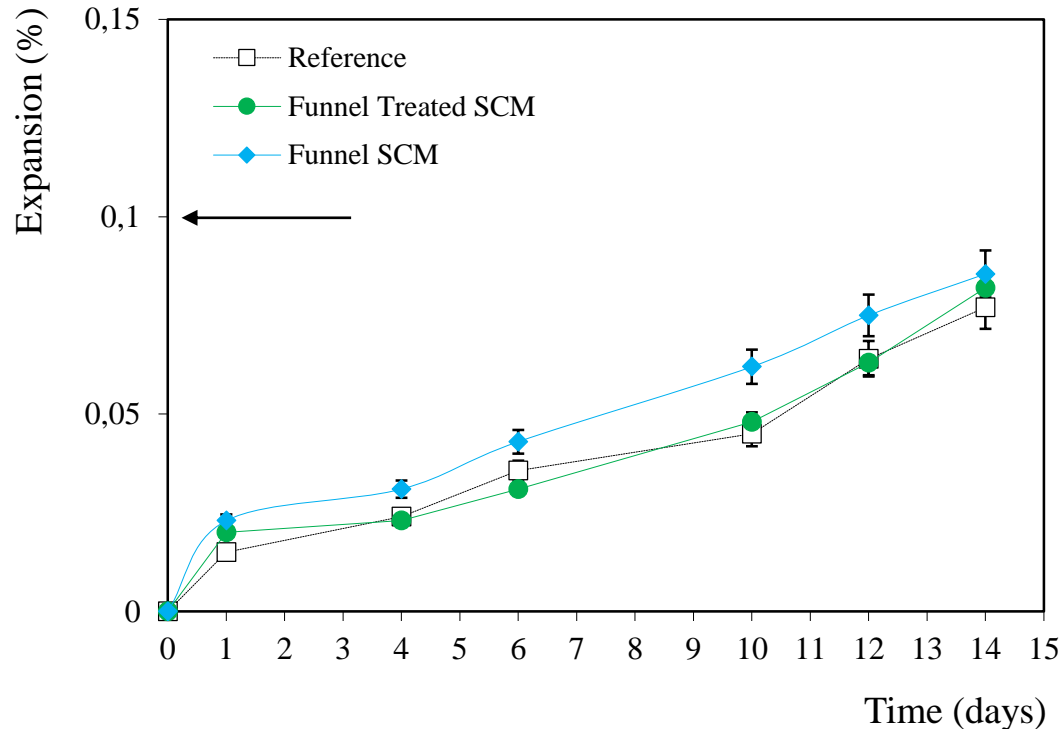
No preferential channel for Pb release were opened by NTA treatment



# FNL glass as SCM

## EXPANSION TEST

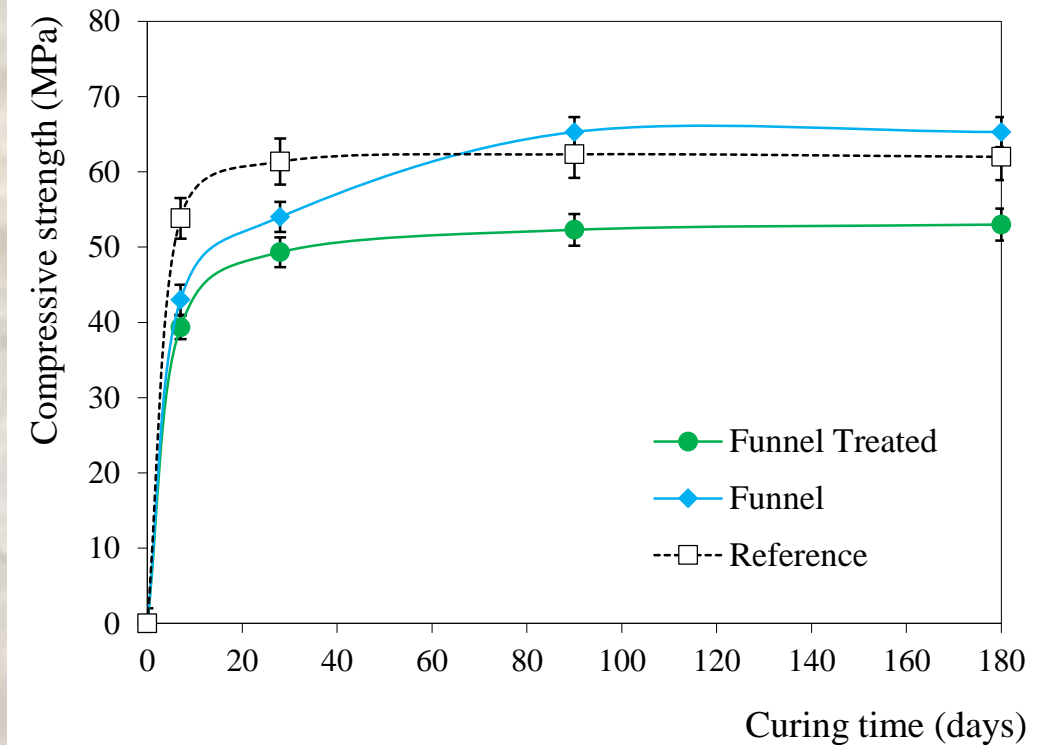
(ASTM C1260 and ASTM C227)



The expansion of the samples is below the safety limit (0.1%) defined by the standards

## MECHANICAL TEST

(EN 196--1)



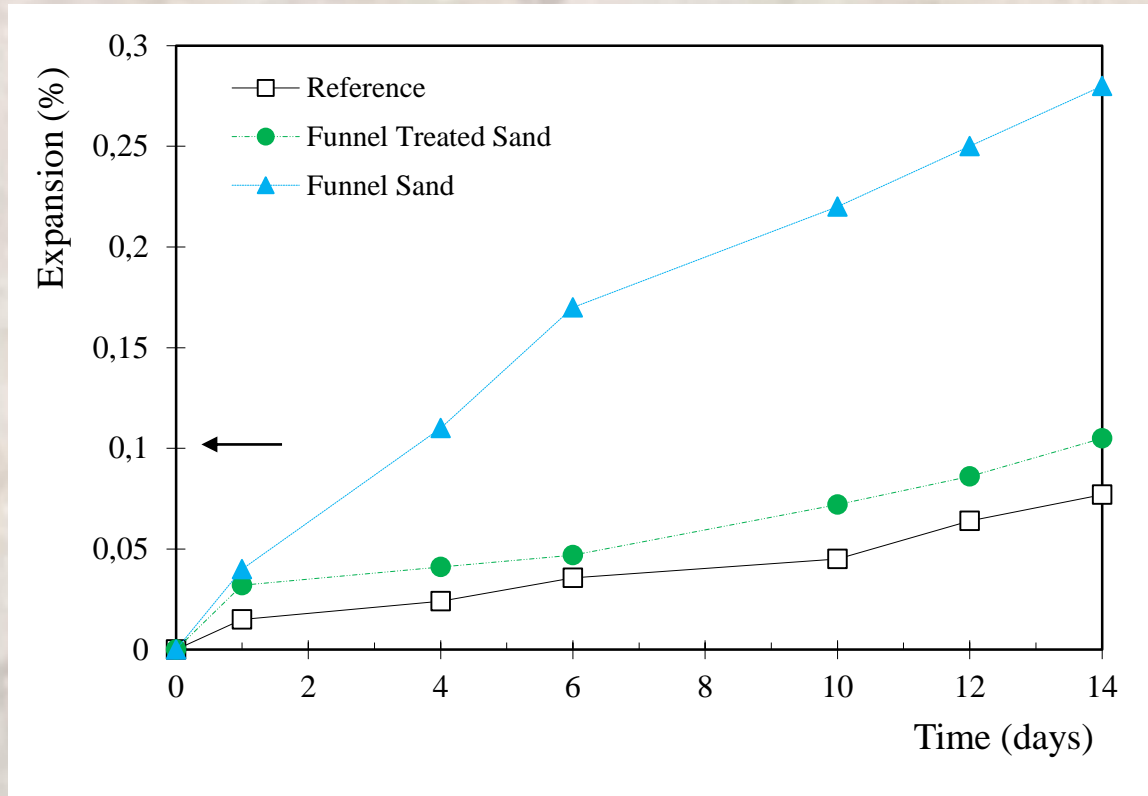
- Untreated funnel glass behaves as an efficient pozzolanic material
- Treated funnel glass instead behaves as a poorly reactive material: the activity index (EN 450-1) is 80 at 28 d and 85 at 90 d (limits for SCM:  $\geq 75$  at 28 d and  $\geq 85$  at 90 d)



# FNL glass as fine aggregate

## EXPANSION TEST

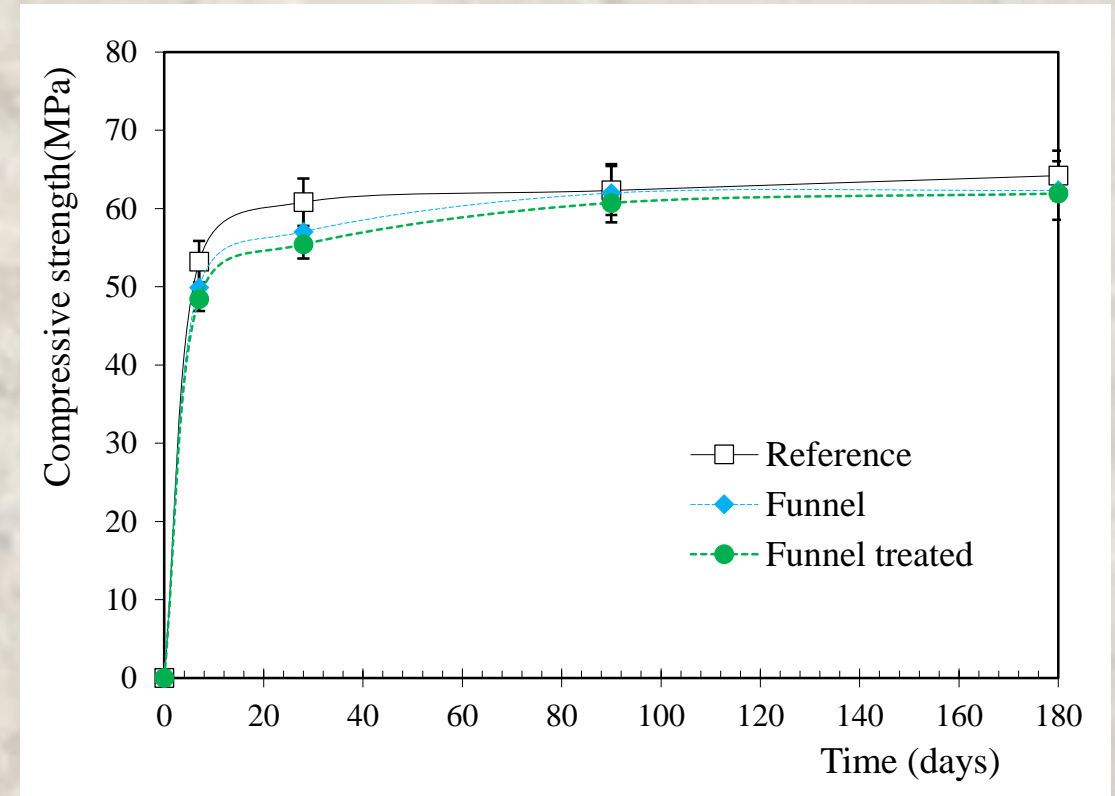
(ASTM C1260 and ASTM C227)



- FNL sand exceeds the limit of 0.1% expansion at 4 days of curing
- Treated FNL shows an expansion comparable to that of the unreactive control sand

## MECHANICAL TEST

(EN 196--1)



- Treated and untreated FNL cause a small reduction of mechanical strength for short curing times (smoother surface of the glass compared to that of natural sand)
- At long curing times the mechanical strength of mortars containing FNL is comparable to the standard

# Conclusions

- A mild, environmentally sustainable treatment based on NTA has been performed on CRT glass to be used in cement mortars.
- NTA treated glass becomes less soluble because of Pb depletion that should reduce the risk of pollution from leaching.
- NTA treatment decreases the pozzolanic activity of the glass, making it a filler material rather than SCM.
- NTA treatment allows its use as fine aggregate in substitution of natural sand suppressing ASR reactions.



THIS APPLICATION IS  
ENVIRONMENTALLY PREFERRED  
SINCE IT REDUCES THE  
ENERGETIC COSTS AVOIDING  
STRONG MILLING PROCESS



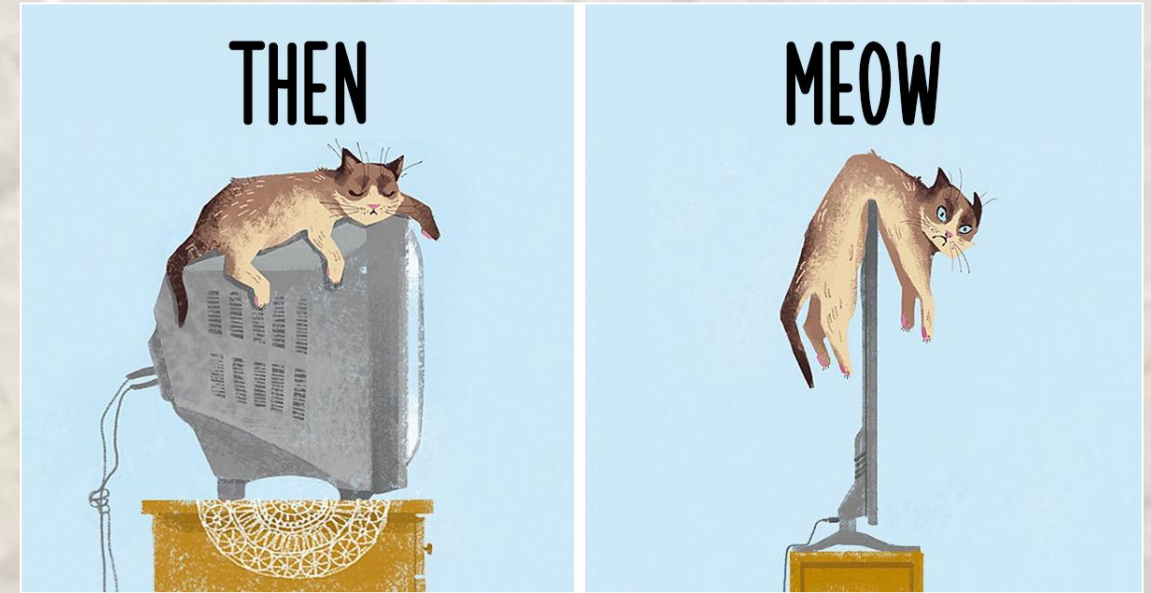
*Thank you for your kind  
attention!*



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