Effect of the active metal supported on SiO₂ to the selective hydrogen production on the glycerol steam reforming reaction

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ABSTRACT

Climate change and the finite nature of fossil fuels have helped the development of biofuels as the only realistic alternative to petro-oil, with biodiesel experiencing an increase of almost 3000% in its production between 2000 and 2012, exceeding 430 thousand barrels per day. One of the more vocal advocates of biodiesel development has been the European Union, setting a target to deliver 10 per cent of energy in transport from renewable sources by 2020, and separately, to reduce the GHG lifecycle emissions of transport fuels by 6 per cent by 2020.

The principal byproduct of the biodiesel industry is glycerol, as every 10 g of oil undergoing the transesterification process produces 1 g of crude glycerol as byproduct, containing a number of impurities that prevent it from being used as raw material in the pharmaceutical and cosmetic industries. Hence, the excess of crude glycerol produced in the biodiesel industry (exceeding 2 million metric tons in 2012) is leading glycerol to be considered as a waste instead of a co-product. The production of hydrogen using glycerol as feedstock is one of the most interesting options, as hydrogen is considered a clean energy source whose demand is expected to greatly increase in the future, mainly due to technological advancements in the fuel cell industry.

Based on this background, a comparative study of catalytic performance for nickel (Ni), cobalt (Co) and copper (Cu) supported on silica catalysts, for the glycerol steam reforming reaction, is reported in this contribution. Catalysts were synthesized applying the incipient wetness impregnation method at a constant metal loading (5 wt. %). The synthesized samples were characterized by N₂ porosimetry (BET method) at their calcinated form and by XRD at calcinated and reduced forms. The chemical composition of the catalysts was determined by ICP, while the deposited carbon on the catalytic surface during the reaction was measured by a CHN analyzer. Catalysts' performance for glycerol steam reforming was studied in order to investigate the effect of the reaction temperature on (i) Glycerol total conversion, (ii) Glycerol conversion to gaseous products, (iii) Hydrogen selectivity and yield, (iv) Selectivity of gaseous products, and (v) Selectivity of liquid products. From the work presented herein, it can be concluded that Ni based on silica catalysts are more active and produce less liquid effluents than Co or Cu based on silica catalysts.

1. Introduction

Arguably, fossil fuels have helped built our current civilization, created our wealth and enriched the lives of billions. But they also have rising costs to our security, economy, health and environment that are starting to erode, if not outweigh their benefits. Recent statistical data from the World Energy Council shows that 82% of the total commercial energy consumed in the world was derived from fossil sources, with the figure being even higher in the transport sector, standing at 98% [1]. Serious concerns about the future availability of those non-renewable fuels, especially oil, have been prominent in public awareness and discourse since the oil crisis of the 1970's [e.g.; 2-4] However, increased anxiety is being caused by the ever growing emissions of manmade greenhouse gases (GHG), caused by the burning of fossil fuels, and the subsequent effects on the planet's climate and biodiversity.

Among the various Renewable Energy Systems (RES) that have been developed, the use of biomass as potential energy provider has gained considerable attention, especially in the field of biofuels, as the only realistic alternative to petro-oil [eg, 5,6]. Figure 1, depicts the world biofuel production from 2007 to 2012. As can be seen, bioethanol production, after reaching a peak in 2010 has experienced a gradual decrease in 2011 and 2012 [7]. Biodiesel production reached a peak in 2011 and stalled in 2012. However bioethanol production still remains more than triple that of biodiesel.



Figure 1. Total biofuels production (biodiesel and bioethanol) in the world in thousands of barrels per day from 2007-2012 [7]

Biodiesel is currently produced from the transesterification reaction between vegetable oils or animal fats (mainly, sunflower, rapeseed oils, palm oil, canola oil, cotton seed, soybean, Jatropha curcas, algae, waste frying oils, non-edible oils) and principally methanol (although ethanol is also used to a lesser extent) in the presence of an acidic or alkaline catalyst to form the biodiesel; fatty acid methyl esters (FAME) or fatty acid ethyl esters, as shown in Eq. 1 [8-10].

$$C_{3}H_{5}(OOC)_{3}(R_{n})_{3} + 3R'OH_{Alcohols} \square 3R_{n}COOR' + C_{3}H_{5}(OH)_{3}$$
(1)

Figure 2 depicts the major biodiesel producing countries in the world. Interestingly, biodiesel production is not dominated by a handful of producers or a particular geographic region (as is the case with oil and natural gas); rather a number of countries have been developing this resource. Although not shown on Figure 2, additional countries such as India, Malaysia, the Philippines, Colombia and Canada have also been notable in increasing biodiesel production.



Figure 2. Major biodiesel producers (%) in 2012 [7]

Over the past decade, biodiesel has moved from being a niche energy source in the European transport sector to being a significant source of road transport fuel, with the EU 27 experiencing an increase in the use of biodisel of over 70% between 2007 and 2012 [7]. Germany and France have mainly bore the brunt of this increase, with Italy, Spain, Austria, Belgium, Netherlands, Portugal and Poland being the next notable producers (Fig. 3). At present, the EU has a target to deliver 10 per cent of energy in transport from renewable sources by 2020, and separately, to reduce the GHG lifecycle emissions of transport fuels by 6 per cent by 2020 [11,12]. Naturally, the pursuit of these twin targets promotes the expansion of biofuels, and mainly that of biodiesel, as bioethanol production in the EU is minimal.

However, since 2012, there has been an intense debate as to how best to address current failings in the policy mechanisms underpinning EU support. This has largely focused on how to ensure that GHG accounting takes proper consideration of the emissions from indirect land use change (ILUC) associated with biofuel feedstock production. There is also recognition that EU policy has led to the adoption of predominantly conventional biofuels, i.e. those using primarily food or feed-based feedstocks reliant on land for their production. Moreover, technological and logistical advances towards biofuels using non landbased feedstocks such as waste and residues have only materialised slowly. These issues are yet to be resolved, with proposed amendments to the relevant legislation currently stalled [13, 14].

In any case, one of the barriers for the further development and commercialization of biodiesel is its high production cost, which is caused by the price of raw materials [15,16]. Thus, the industry needs to find new and innovative ways of maximizing its profits either by bringing down

the cost of raw materials (hence the move towards making use of waste cooking oils) and/or by making use of its existing waste streams.



Figure 3. EU-27 biodiesel production in thousand of barrels per day from 2007-2012 [7]

The principal byproduct of the biodiesel industry is glycerol, as every 100g of oil undergoing the transesterification process produces 10g of glycerol as byproduct. The glycerol so obtained is crude as it contains non-reacted and partially reacted fats, free fatty acids, methanol, esters and salts, and thus, it cannot be used as raw material in the pharmaceutical and cosmetic industries [17]. A viable solution could be the reconstruction of biodiesel plants into novel biorefineries through the integration of glycerol-based bioconversions in existing lines for the production of various chemicals [18] or the production of synthesis gas and hydrogen [19]. Moreover, it is important to note that the excess of crude glycerol produced (Fig. 4) in the biodiesel industry (exceeding 2 million metric tons in 2012) is leading to a decrease in glycerol prices, with glycerol now being considered as a waste instead of a co-product [20].

The production of hydrogen is one of the most interesting options, as hydrogen is considered a clean energy source and has numerous uses. Moreover, the demand for hydrogen is expected to greatly increase in the future, mainly due to technological advancements in the fuel cell industry [21,22]. At present, almost half of the hydrogen produced worldwide is generated through the steam reforming of methane (SRM), with the reforming of naphtha/oil accounting for 30%, coal gasification for 18% and electrolysis for only 4% [23]. Hydrogen can be produced from glycerol by catalytic steam reforming (SR) [e.g. 24-28], oxidative steam reforming [29], autothermal reforming (ATR) [30,31], aqueous phase reforming (APR) [32-35], and supercritical

water (SCW) reforming [36-38]. However, the reaction that has attracted most attention is that of the steam reforming, partially due to the fact that the process is widely used in industry, and would require only minor alterations in existing systems if the feedstock was changed from natural gas or naphtha to glycerol [23].



Figure 4. World and EU-28 glycerol production in millions of tones per year from 2007-2012 (calculations based on an average biodiesel density of 0.86 g/cm³)

Based on this background, a comparative study of catalytic performance for nickel (Ni), cobalt (Co) and copper (Cu) supported on silica catalysts, for the glycerol steam reforming reaction, is reported in this contribution. Catalysts were synthesized applying the incipient wetness impregnation method at a constant metal loading (5 wt. %). The synthesized samples were characterized by N₂ porosimetry (BET method) at their calcinated form and by XRD at their calcinated and reduced forms. The chemical composition of the catalysts was determined by ICP, while the deposited carbon on the catalytic surface during the reaction was measured by a CHN analyzer. Catalysts' performance for glycerol steam reforming was studied in order to investigate the effect of the reaction temperature on (i) Glycerol total conversion, (ii) Glycerol conversion to gaseous products, (iii) Hydrogen selectivity and yield, (iv) Selectivity of gaseous products, and (v) Selectivity of liquid products.

2. Experimental

2.1 Catalysts preparation and characterization

The silica support, which was obtained from Englelhard (SDS code: SI-1624E) in powder form, was first pelletized and then crashed and sieved to 350-500 μ m, before being calcined at 800 °C for 4 h. The catalysts were prepared via the incipient wetness impregnation method, by impregnating the SiO₂ with Ni(NO₃)₂ 6H₂O, CO(NO₃)₂ 6H₂O and Cu(NO₃)₂ 6H₂O, aqueous solutions having the appropriate concentration, in order to obtain 5 wt. % Ni, Co and Cu

respectively in the final catalysts (the catalysts were labeled as Ni/Si, Co/Si and Cu/Si). The total volume of the impregnation solutions was equal with the total pore volume of the silica used. The impregnated samples were dried overnight and calcined at 800 °C for 5 hours. All solutions for the catalysts preparation utilized distilled and deionised pure water generated by NANOpure Diamond UV unit (Barnstead International).

Surface areas (S_{BET}) of the catalytic samples were determined by the N₂ adsorption–desorption isotherms at -196°C using the Nova 2200e (Quantachrome) flow apparatus, according to Brunauer-Emmett-Teller (BET) method at the relative pressure in the range of 0.05–0.30. The total pore volume calculation was based on nitrogen volume at the highest relative pressure, whereas the average pore size diameter was determined by the Barrett-Joyner-Halenda (BJH) method. Prior to the measurements the samples were degassed at 350 °C for 5 h under vacuum.

The total metal loading (wt. %) of the final catalysts was determined by Inductively Coupled Plasma Atomic Emission Spectroscopy (ICP-AES) on a Perkin-Elmer Optima 4300DV apparatus. The wavelengths selected were at 341.476, 227.022, and 231.604 nm. The selected conditions of the measurement were: Plasma flow: 15 L/min, Auxiliary flow: 0.2 L/min, Nebulize flow: 0.6 L/min, RF Power: 1300 watts, Plasma View: radial view, and Sample Flow Rate: 2 mL/min. The acid digestion procedure involved the weighting of each sample to the nearest 0.00001 g in a Teflon beaker and its transportation to a fume hood, where 1 ml of concentrated sulphuric acid was added. The mixture was then heated to dryness at low heat on a hot plate overnight. Afterwards, 2 ml of concentrated hydrochloric acid and 2 ml of concentrated nitric acid were added to the beaker with the heating being terminated after 5-10 min, when the reaction of dissolution was completed. At this point, about 2 ml of de-ionized water were added and the beaker was left to cool. The resulting clear solution was loaded carefully in a 50 ml volumetric flask in order to make up an accurate fixed volume adding de-ionized water. Each sample was measured thrice, in order to check repeatability.

The catalysts' crystalline structure was determined by applying the X-ray diffraction (XRD) technique, using a ThermoAl diffractometer at 40 kV and 30 mA with Cu K_a radiation (λ =1.54178 nm). Diffractograms were recorded in the 20=2-70 range at a scanning rate of 0.04 over 1.2 min-¹. The diffraction pattern was identified by comparison with those of known structure in the JCPDS (Joint Committee of Powder Diffraction Standards) database. It should be noted that the XRD technique was used for both fresh and reduced samples.

The percentile concentration of carbon in the used catalysts was measured by quantitative infrared spectroscopy performed with a Leco CHN-200 analyser, using 0.1 g of each sample.

2.2 Catalytic performance

The glycerol steam reforming reaction was carried out at atmospheric pressure, in a continuous flow, fixed-bed, single pass, tubular stainless steel reactor, with an inner diameter of 14 mm, at temperature ranging from 400-750 °C (Fig. 5). The experimental set up used allowed the feeding of both liquid and gaseous streams, having two vaporizers and a pre-heater before the reactor and a condenser after it. The vaporizers, pre-heater and reactor are placed into electrical ovens and regulated with programmed-temperature controllers.

The liquid stream consisted of $C_3H_8O_3$ (20% w.w.) and H_2O (total liquid flow rate = 0.12 ml/min). The glycerol used had 99.5% purity and was obtained from Sigma Aldrich. The glycerol/ water mixture was fed with a HPLC pump (Series I) and was first vaporized at 350°C before it was mixed with He (He flow rate = 38 ml/min). The reactor's outlet gases passed through a cold trap for liquid products capture. Prior to catalytic testing, 200 mg of catalyst was reduced in situ in a hydrogen flow (100 ml/min) at 800 °C for 1 hr. The gaseous products were analyzed on-line by a gas chromatographer (Agilent 7890A), with two columns in parallel, HP-Plot-Q (19095-Q04, 30 m length, 0.530 mm I.D.) and HP-Molesieve (19095P-MSO, 30 m length, 0.530 mm I.D.), equipped with TCD and FID detectors. Liquid products were analyzed via a combination of Gas Chromatography (Agilent 7890A, with a 5MS column, equipped with an FID detector) and Mass Spectroscopy (Agilent 5975C).



Figure 5. Schematic flow chart of experimental setup for activity test of catalysts towards glycerol steam reforming

Catalytic performance is reported in terms of H₂ yield, H₂, CO, CH₄ and CO₂ selectivity, glycerol conversion into gaseous products, and total glycerol conversion (global conversion). Moreover, the performance of the catalysts in the liquid phase is reported in terms of acetol (C₃H₆O₂), acetone [(CH₃)₂CO], allyl alcohol (CH₂=CHCH₂OH), acetaldehyde (C₂H₄O) and acetic acid (C₂H₄O) selectivity. Performance parameters were calculated based on the following equations:

$$\% glycerol \ conversion_{(global \ conversion)} = \left(\frac{Glycerol_{in} - Glycerol_{out}}{Glycerol_{in}}\right) \times 100$$
(2)

$$\% glycerol \ conversion_{(gaseous \ products)} = \left(\frac{C \ atoms \ in \ the \ gas \ products}{total \ C \ atoms \ in \ the \ feedstock}\right) \times 100$$
(3)

$$H_2 \text{ yield} = \frac{H_2 \text{ moles produced}}{\text{moles of glycerol in the feedstock}}$$
(4)

$$\%H_2 \ selectivity = \left(\frac{H_2 \ moles \ produced}{C \ atoms \ produced \ in \ the \ gas \ phase}\right) \times \left(\frac{1}{RR}\right) \times 100$$
(5)

where, RR is the reforming ratio (7/3), defined as the ratio of moles of H_2 to CO_2 formed.

% selectivity of
$$i = \left(\frac{C \text{ atoms in species } i}{C \text{ atoms produced in the gas phase}}\right) \times 100$$
 (6)

where, species i refers to CO, CO₂ and CH₄.

% selectivity of
$$i' = \left(\frac{C \text{ atoms in species } i'}{C \text{ atoms produced in the liquid phase}}\right) \times 100$$
 (7)

where, species i' refers to acetol, acetone, allyl alcohol, acetaldehyde and acetic acid.

3. Results and discussion

3.1 Characterisation results

In Table 1 the physicochemical properties of all samples are presented. As can be observed, the specific surface area (SSA, i.e., S_{BET}) and the pore volume (Vp) for all catalysts is lower than the one of the supporting material. The lower surface area can be attributed to the fact that the internal surface area of the support pore system is probably progressively covered by nickel, cobalt and copper species adsorbed on silica's active sites forming a layer [39]. Nonetheless, it is worth pointing out that all three samples have comparable SSA and Vp to one another. Moreover, the ICP results (metal loading) indicate that the desired metal levels were achieved for all samples.

I able 1. Physicochemical properties of the calcinated samples					
Sample	S _{BET} (m²g⁻¹)	V _p (ml g⁻¹)	Metal loading ICP (wt%)		
SiO ₂	108.27	0.86	-		
Ni/Si	84.09	0.69	4.86		
Co/Si	87.01	0.74	4.73		
Cu/Si	71.92	0.64	4.85		

Figure 6 depicts the XRD patterns of the Ni/SiO₂ catalyst after calcination and after reduction. Characteristic peaks at 2θ =21.9°, corresponding to SiO₂ (Cristobalite) and 2θ =26.5° corresponding to SiO₂ (Quartz) are observed for both samples. The nickel oxide (NiO) structure was detected at 2θ =37.2° and 43.2° on the calcined sample, while on the reduced sample we observed the appearance of two small peaks due to the presence of metallic nickel (Ni⁰) at

 2θ =44.3° and 51.7°. Figure 7 depicts the XRD patterns of the Co/SiO₂ and Cu/CiO₂ catalyst after reduction. SiO₂ (Cristobalite) and SiO₂ (Quartz) where observed for both catalysts at the same 2 θ as above. Metallic cobalt (Co⁰) was detected at 2θ =44.05° and 51.4° for the Co/Si sample, and metallic Cu (Cu⁰) at 2θ =43.24° and 50.36° for the Cu/AI sample. The crystalline phases that were detected for the SiO₂ support and for the catalysts in their calcinated and reduced forms are summarized in Table 2.



reduced (at 800°C) Ni/Si catalysts



Table 2.	Crystalline	phases of	support and	d catalysts
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Sample	Crystalline phases
SiO ₂ (c)	SiO ₂ (Cristobalite), SiO ₂ (Quartz)
Ni/Si (c)	SiO ₂ (Cristobalite), SiO ₂ (Quartz), NiO
Ni/Si (r)	SiO_2 (Cristobalite), SiO_2 (Quartz), Ni
Co/Si(c)	SiO ₂ (Cristobalite), SiO ₂ (Quartz), Co ₃ O ₄ , Co ₂ SiO ₄
Co/Si (r)	SiO ₂ (Cristobalite), SiO ₂ (Quartz), Co
Cu/Si (c)	SiO ₂ (Cristobalite), SiO ₂ (Quartz), CuO
Co/Si (r)	SiO ₂ (Cristobalite), SiO ₂ (Quartz), Cu

Note: c=calcinated, r=reduced

3.2. Catalytic activity and selectivity

Thermodynamic studies predict that high temperatures, low pressures and high H_2O/C ratio favor hydrogen production. A number of researchers suggest that the ideal condition to obtain hydrogen is at reaction temperatures between 627 and 700 °C, with a molar ratio of water to glycerol higher than 9. Under these conditions, methane production is minimized and carbon formation is thermodynamically inhibited. Although excess water allows higher selectivity to hydrogen, a significant water amount in reaction products is not beneficial [24,25,40-43]. Thus, in this work, reaction tests were carried out in a temperature range of 400-750 °C, at atmospheric pressure and for a water-glycerol molar ratio of 20:1.



Figure 8. Total glycerol conversion and glycerol conversion into gaseous products for the Ni/Si, Cu/Si and Co/Si catalysts



Figure 9. Hydrogen yield and selectivity for the Ni/Si, Cu/Si and Co/Si catalysts

Glycerol total conversion and glycerol conversion into gaseous products is presented in Figure 8. As can be clearly observed, all three catalysts show improvements with increased temperatures, which is a consequence of the endothermic nature of the overall steam reforming reaction; however, the Ni/Si catalyst exhibits significantly higher conversions into gaseous products. In fact, as can be observed from Figure 8, the sequence of catalytic performance is Ni/Si>Co/Si>Cu/Si. Glycerol total conversion is essentially flat for all the catalysts, with the Cu/Si sample performing the worse. It should be noted that this high glycerol total conversion has been observed by all researchers concerned with this reaction [e.g. 26,44].



Figure 10. CO₂, CO and CH₄ selectivity for the Ni/Si, Cu/Si and Co/Si catalysts

The GC analysis revealed that the gaseous products were H_2 , CO_2 , CO and CH_4 , which is in line with previous work by other researchers that have also indicated that above reaction temperatures of 400 °C these gases are the major products of glycerol steam reforming [45-49]. Hydrogen yield and selectivity (%) are presented in Figure 9. Hydrogen selectivity increases with increasing temperatures for all catalysts however, their behavior is not similar to one another. The selectivity for the Cu/Si sample begins at low values ($\approx 25\%$) at 400 °C, and increases sharply up to 500 °C; from then on it almost plateaus. On the contrary, for both Ni/Si and Co/Si samples, hydrogen selectivity has high initial values ($\approx 70\%$ and $\approx 50\%$ respectively), but the increase is very gradual, also almost terminating at 500 °C. The sequence of catalytic performance, in terms of H_2 yield (moles), is again Ni/Si>Co/Si>Cu/Si (Fig. 9). It is noteworthy however that although the Co/Si sample exhibits higher hydrogen yield than the Cu/Si sample between 400-600 °C, above this temperature the two catalysts have similar selectivity's.

The selectivity of CO_2 , CO and CH_4 for all three catalysts is presented in Figure 10. For all three catalysts, the formation of CH_4 is considerably low during the whole test, which can be attributed to the steam reforming of methane derived from glycerol decomposition [28]. For the Ni/Si

sample, CO₂ selectivity decreases up to 650 °C and then it experiences a relatively sharp increase; the opposite is true for CO selectivity, i.e., it increases up to 650 °C, before decreasing. For the Co/Si catalyst, carbon monoxide and carbon dioxide selectivity exhibit a volcano and reverse volcano type behavior, between 550-700 °C. The CO₂ selectivity for the Cu/Si sample has a very slight downward slope during reaction, while CO selectivity a gradual upward trajectory. It is noted that the presence of CO in the gas mixture is significant, as it can adversely affect the performance of both anode and cathode in proton-exchange fuel cells (PEMFCs) acting as poison [50,51].





Figure 11. Liquid products' selectivity for the Ni/Si catalyst

Figure 12. Liquid products' selectivity for the Cu/Si catalyst



Figure 13. Liquid products' selectivity for the Co/Si catalyst

Condensed reaction products (liquid products) presented a yellowish colour and by combined gas chromatography and mass spectroscopy (CG/MS), a number of compounds were identified

and quantified. The compounds identified for all three catalysts were acetic acid, acetaldehyde, allyl alcohol, acetone and acetol. For the Ni/Si catalyst these products where present mainly at relatively low temperature ranges, i.e., from 400 - 600 °C (Fig. 11), which can be attributed to the different reaction routes that convert glycerol to liquid products (e.g. glycerol hydrogenolysis) that are exothermic in character [41]. However, for both the Cu/Si and Co/Si samples (Figs. 12 and 13 respectively), liquid effluents were produced throughout the catalytic testing (i.e., from 400 - 750 °C).

Sample	Carbon (%)
Ni/Si	23.62
Co/Si	9.97
Cu/Si	12.65

Table 3. Carbor	concentration	in the used	d catalysts
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Unfortunately, studies on carbon deposition over Ni-based catalysts and the mechanism of coke formation for the steam reforming of glycerol are still missing in the literature. However, some contributions have reported the deactivation of Ni-supported catalysts on SR of glycerol and associated this phenomenon with the formation of both highly reactive carbon species and low reactive, more ordered structures, particularly filamentous carbon [25,26,41,48,52]. This can probably provide an explanation for the results depicted on Table 3, of the percentile concentration of carbon as measured on the used catalysts, where despite the fact the Ni/Si catalyst exhibits a better catalytic performance that the other two samples, more carbon has been deposited on its surface.

4. Conclusions

The need to move from fossil based resources in the transport sector led to the promotion of biofuels as the only realistic alternative to petro-oil. However, the increase in biodiesel production has been accompanied by increases in glycerol production, which is the main by-product of the process. As the production of glycerol exceeded 2 million metric tons in 2012, it is now considered as a waste instead of a co-product. Arguably, glycerol valorization to hydrogen is one of the prospective ways to alleviate our dependence on fossil fuels and mitigate this waste management issue with heterogeneous catalysis playing a critical role in converting glycerol to a valuable product.

From the work presented herein, it can be concluded that Ni based on silica catalysts are more active and produce less liquid effluents than Co or Cu based on silica catalysts.

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